The bug zapper

A bachelor's report

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Killing mosquitoes using acoustical source localisation and a

laser to shoot them.



Summary

In this project the goal was to improve the bug zapper that Ruud van Laar and Martijn van der Ouderaa started with. The sound localisation had to be improved and the laser had to be implemented.

The sound localisation is still done by five microphones, with one of them as reference microphone. We improved the set-up by changing the positioning of the microphones. The average error in the x-direction is 1.1 cm (maximum 3.5 cm), in the y-direction it is 0.6 cm (maximum 2.6 cm) and in the z-direction it is 1.0 cm (maximum 2.4 cm). The measurable space is approximately spherical, with a diameter of 15-20 cm. The calculation time is a 130 times faster, which is mainly due to the substitution of the Matlabnodes by Labview functions and a shorter sample length.

The laser is controlled with a two-axis galvano-system. The combining of these two parts is simple, the output from the sound localisation is the input for the galvano-system. The total success rate of our device is 85%, which means that only 15% of the mosquitoes that fly through the measurable space will survive.

Table of Contents

Introduction	4
Theoretical aspects	5
Sound source	5
Sound localisation	5
Laser & Galvano-mirrors	7
Complete device	9
Error analysis	9
Experimental aspects	10
Sound source	10
Microphones & calibration	10
Galvano-mirrors	10
Complete device	12
Results	13
Sound source	13
Microphones & calibration	13
Sound localisation	18
Galvano-mirrors	20
Complete device	23
Discussion	24
Sound source & sample	24
Sound localisation	24
Galvano-mirrors	24
Processing time	24
Laser	25
Complete device	25
Conclusion	26
Recommendations	27
List of abbreviations	
References	29

Introduction

'But why would you want to do that?' is a question that many researchers will hear way too often when they introduce their research problem. During our bachelor thesis, we have never heard this question, because the answer is well-known and the problem we would like to solve is a problem that every human being has had at least once in their life.

The goal of our project is to finish the bug zapper that two other students started with this year. A bug zapper is a system that kills bugs (and in this project especially mosquitoes) by detecting the location of its sound and kills it by shooting it with a laser beam.

We had the sound localisation, make it real-time and add a laser-device that will shoot at the location of the sound source or, in a real scenario, kill the mosquito. Though humans easily locate a sound just by ear, it is not that easy to determine the location using microphones. There are different kinds of algorithms, but not all of them are fast enough or applicable in our situation.

We have improved the source localisation that Martijn van der Ouderaa and Ruud van Laar started with and use the same algorithm. The changes we made to their set-up and techniques will be discussed in the chapter 'theoretical aspects'. There we will also discuss the theoretical aspects of the laser and the galvano-mirrors.

The implementation and of the laser and scanners will be discussed in the experimental aspects. The limitations of our set-up will be discussed in this part as well as the computation time.

In the chapter 'results' the measurements will be analysed, which will lead to a discussion and conclusion and some recommendations to improve the set-up and kill even more mosquitoes.

Theoretical aspects

To make a fully functioning bug zapper, we have to improve the previous design at various points. In general we can say that there are four steps to work through:

- 1) Improve the sound localisation such that its deviation is smaller than the size of a mosquito and try to reduce the processing timeⁱ.
- 2) Make the laser shoot the sound source accurate and fast enough.
- 3) Combine these two systems and test the speed of the combined device; it has to be fast enough to shoot the mosquito before it moved too far away from the detected location.
- 4) Test the accuracy of the combined system.

Sound source

The mosquito sound used to determine the location is the same audio file as Ruud van Laar and Martijn van der Ouderaa used in their experiment. [4] The base frequency in this signal is around 375Hz, with a second harmonic around 750Hz and the third harmonic around 1125Hz [1].

Because the sound source is considered to be a point source, the distance between the source and the microphones should be much bigger than the diameter of the source. Therefore a smaller sound source is used and the precision of this source will be compared with the precision of the source with a diameter of 5 cm.

Sound localisation

As said before, the deviation of the sound localisation has to be smaller than the size of a mosquito. In the case of normal mosquitoes this means that the maximum deviation is approximately 0.5 cm, but this deviation is the maximum deviation for a non-moving object. Since a mosquito flies around with a speed of 0.5 m/s [2], the mosquito will change its location during measurements and calculations. The time of the measurement plus the time of the localisation process has to be shorter than the time it takes the mosquito to fly 0.5 cm minus the deviation of the device. It is easily seen that the maximum time we have for calculations and measurements is about 0.01 sec.

For the localisation we will use the same algorithm as Ruud van Laar and Martijn van der Ouderaa: the linear closed form algorithm as explained by M.D. Gillette and H.F. Silverman [3]. They had good results with this algorithm, but we will have to change the method of using it. They averaged over 100-200 measurements, while we have to use one single measurement to reduce the processing time. To obtain the same accuracy as they had, we will have to improve the accuracy of each measurement.

This algorithm determines the location of our source only in the near field, which means that the difference in the time of arrival must be significant. This is good enough for our system, since it is about 50 cmx50 cmx50 cm. For more detailed information about this algorithm we refer to the paper

ⁱ Since we have to measure the incoming sample, we will never be able to make the sound localisation real time, but we have to make it as fast as possible.

[3], briefly, it calculates the location of a sound source out of the difference between the distance to four detectors and one reference detector.

This method needs five microphones, the sound will arrive at the microphones with a short delay relative to the reference microphone. This will be called the Time Difference Of Arrival (TDOA) and from this time the Distance Difference Of Arrival (DDOA) can be calculated.

We might place the microphones in a different way compared to the original set-up [1]. Their recommendations mentioned: "We positioned the microphones in a way we expected to be good for measuring the TDOAs, but it is again not guaranteed that this is the optimal solution. To find the ideal positioning would require further study on the algorithm or trial and error." [1].

A disadvantage of repositioning the microphones is that we have to redo the measurements for the compensation of the errors in the DDOA [1], but this is only a calibration of the system, we can keep the vi-file that executes the algorithm. We will try to find out the best way to place the microphones by trial and error, because we do not know exactly what causes the errors in the measurements.

In the original set-up, the microphones were placed behind the space that was measured in. We will call this plane the y-z plane. We decided to surround the space that was measured in, because we noticed that the measurements in the x-direction were less stable than the measurements in the y-and z-direction. The difference between these set-ups is shown in figure 1, where you can see that mainly in the x-direction the microphones are more spread.





Figure 1: Above the old set-up and below the new set-up

Laser & Galvano-mirrors

In our set-up we used a laser in combination with a two-axis galvano-mirror to target the mosquito after pinpointing its position using the acoustical localisation algorithm. The galvano-mirror is a device with two mirrors on two different axes which are mounted on two individually controllable motors. By rotating the mirrors the angle of incidence and therefore the angle of reflection of a beam aimed at the mirrors can be changed. Figure 2 shows the two galvano-mirrors.



Figure 2: The galvano-mirrors.

Because the mosquito is moving, a fast response of the mirrors is necessary. To characterise the dynamic response of the galvano-mirror the step response has been measured. We need the step response of the galvano-system, because we want to shoot as fast as possible at the location of the mosquito directly after measuring its location. After an initial targeting the galvano-mirrors will have to track the mosquito at a low speed. Therefore this behaviour can be considered quasistatic. To analyse how fast and precise this step response is, we measure the response of the motor that rotates the mirror. The step response can be characterized by multiple parameters, we will use the following:

- Step amplitude
- Settling time: the time it takes for the beam to coincide with the input value within the beam width
- Input delay: the time difference between the moment of input to the galvano-mirrors and the moment of motion of the galvano-mirrors
- Response time: the sum of the settling time and the delay
- Overshoot: a non periodic ripple

The (step) response depends on the physical and electrical properties of the electronics, the motor and feedback sensors. We use a hardware that is a commercially available kit, AXJ-V20, used for laser shows. The available documentation is very limited, so we have to measure all of the above described parameters.

The step response of the system can be attributed to the two parts of the system: the DAQ and the galvano-system. The galvano-system consists of an electronic circuit with feedback loop, which controls the galvano-system. In order to separate the step response behaviour of the DAQ and the galvano-system the output of the DAQ will also be monitored. This set-up is schematically shown in figure 3.



Figure 3: Galvano-system schematics

There are two possibilities for the input modes of the galvano-system. The angle of the mirror either has a linear angular response to the input or it has an angular response that is an inverse tangential. The second response sounds counterintuitive from a physicist's point of view, but since we use a system that is build to be used in laser shows where you project an image on a flat screen, it is not strange to have this response. For this application it is useful to have a y-z input because then the user only needs to enter the coordinates of the points of the image, without having to correct for the fact that the image is not projected on a spherical shell rather than on a flat screen. In our case however, the maximum angular deviation of the galvano-mirror is small enough to neglect the difference between these two and just treat the system as a system with y-z input.

The control between an input of spatial coordinates and the output of two voltages has three steps:

- 1 Coordinate transformation
- 2 Projection on calibrated plane
- 3 Transformation to voltage

Suppose that the mosquito is at (x,y,z). The coordinates are transformed to a new coordinate system, (x',y',z'), this coordinate system has its centre on the galvano-mirror with the x'-axis parallel to the equilibrium position of the laser beam. Then we project the (x',y',z') on a new plane, x''. This projection is schematically shown in figure 4. If we know the coordinates in our calibrated plane, we have to transform these coordinates to an input voltage, V.



Figure 4: Scheme of the transformation to the coordinates on the calibrated plane

Because the galvano-mirrors do not have a specified response they have to be calibrated first. In order to do this measurement the y''(V) and z''(V) responses are measured with a fixed x'' distance. By finding the inverse of this relation we get a proper V(y'') relation to use in step 3 of our coordinate to voltage transformation.

Complete device

The complete device consists of the two main parts: the galvano-mirrors and the sound localisation. The coupling between these two sounds easy, the output from the sound localisation has to be transformed and becomes the input for the galvano-mirrors. This is schematically shown in figure 5. The only problem that might occur during this process is that the sum of the measuring and the processing time is too high to hit the sound source. If this is the case we will try to reduce the processing time of both systems to make a functional bug zapper.





Error analysis

The errors in our system will be introduced by the two main parts of the set-up. The sound localisation will not be perfect, as we know from the original set-up for the sound localisation [1]. This will introduce the first error in our system, which will inflect the positioning of the laser beam. The laser beam might also deviate from the position it is meant to be as a result from an error in the galvano-systems. The errors in these two systems together have to be smaller than half the size of the mosquito, which results in a maximum error of 0.5 cm.

Experimental aspects

Some parts of the set-up already existed. We used the same microphones as Ruud van Laar and Martijn van der Ouderaa. Since they were able to measure the location pretty well, we did not expect any problems on this point. The other thing we will use is the VI-file with the algorithm to calculate the location.

Sound source

The easiest way to check if our smaller sound source works better than the sound source with a diameter of 5 cm is to test them both at multiple locations, especially near the microphones, and check whether the result is stable and whether it is reproducible. We also check if the smaller speaker is a good sound source for all of the frequencies of the sample we use.

Microphones & calibration

We optimize the positioning of the microphones by trial and error. We compare the signals of four different microphones with the same reference microphone, which gives us the chance to analyze the differences between the various positions we can choose. We calculate the DDOA between the microphones and compare that to the measured DDOA. We already know that there is a systematic mistake in this measurement [1], which we will obtain from these measurements.

The optimal set-up will be chosen by calculating the standard deviation and the average of the error in the DDOA. The error in the DDOA will be measured for multiple locations of the sound source for the four microphones compared to the reference microphone. The average of the error will be used as a constant correction of the DDOA, Ruud van Laar and Martijn van der Ouderaa already showed that there was an inexplicable error in the DDOA. The set-up with the smallest standard deviation is the most accurate in calculating the DDOA and therefore the best in calculating the location. We will try different ways of positioning the microphones, after doing the calculations for the previous setup. For example, if we conclude that microphones close to each other give better results than the microphones far away from each other, we will try a new set-up with the four microphones closer to the reference microphone.

Galvano-mirrors

To measure the step response of the galvano-mirror a reference timescale is needed. There are multiple methods to do this. One could for example create a square wave and use a chopper to modulate the laser output and use this to scan the output signal. However, by using the fact that the system uses a two-axis galvano-mirror it is possible to create a reference timescale with one galvano-axis and use that to scan the response of the other axis.

One of the galvano-mirrors will be driven with a triangular signal, the other will create a square wave, $\frac{1}{2}\pi$ out of phase with the triangular signal. This will create a step response on a fixed position, and by introducing a small extra phase shift to the square wave the "step up" and "step down" can be separated. This is illustrated in figure 6. By changing the amplitude of the square wave the step response can be characterized.



Figure 6: Simulation of a step response with and without phase difference.

The timescale on the x-axis follows from the frequency (f) of the triangular signal and the width (w) of the signal on the screen as shown in equation 1.

$$dt = \frac{dx}{2 w f} \quad (1)$$

If the frequency is low enough to consider the square wave as a train of independent step functions, it is possible to say that the preceding step function does not influence the next step. We can check whether this is the case by looking if the line of the image is perfectly flat before it bends and use the described method to analyse the step response if the frequency is low enough. If there is some resonance present that is not fully damped before the next step and the resonance frequency is a multiple of the square wave frequency, this resonant signal can be amplified over multiple steps, thus making its influence seem bigger than it would be on not correlated random steps.

However, there might be some other disadvantages using this method. Equation 1 assumes that the galvano-mirror produces a perfect triangular output, this will not be the case. Because the derivative of a triangle is a square function the acceleration would have to be a delta peak at the top of the triangle, which is physically impossible. The triangular and the square wave are $\frac{1}{2}\pi$ out of phase, which means that the angular velocity is constant at the point where the square wave changes sign. We assume that a constant angular velocity as input gives the galvano a constant angular response as output and that the settling time for the change in angular velocity is not too large. From these assumptions we can conclude that the deviation from a delta peak acceleration does not influence the timescale at x=0, but we will have to check if these assumptions are true. If we align the input signal with a $\Delta \varphi = \frac{1}{2}\pi$, the actual projected image shows a slightly different

phase shift between the square wave and the triangle. This phase shift difference has been measured and documented as the input delay.

To measure the input delay in the triangular signal caused by the electronics we used a triangular signal as input signal. By using a photodiode coupled to an oscilloscope situated at the equilibrium position of the beam we measured the delay between the moment that the beam crossed the centre position and the moment that the electrical input to the galvano-system crossed the centre position. From this measurement we can conclude which part of the phase shift between the triangle function and the square function is attributable to the triangle function, if we assume that the lag of the detector is negligible.

Complete device

To test the functionality of the complete device, we will have to move the sound source through the measurable space with the speed of a mosquito. To test the device, we will capture a movie while moving the sound source through the measurable space. We will go through the measurable space repeatedly, and analyse whether the source is hit or not. We will also analyse 60 random shots to determine if the sample is hit or not. From these two analyses we can conclude how accurate our set-up is.

In order to reduce the processing time of the vi-file, we replaced all of the Matlab-scriptnodes by Labview functions. The processing time of the original vi in combination with our vi to control the laser was 0.18 seconds, after changing it was 0.13. This was at a sample length of 10000 and a sample rate of 80000 samples/sec. In order to decrease the processing time even more, we changed the sample length to 1500, but we did not change the sample rate. This gives us a time of 0.019 seconds for the measuring and the processing together. During the measurement, the mosquito can move about 0.95 cm, but the measured position is the position halfway during the measurement, so the deviation is about 0.47 cm, this is smaller than the 0.5 cm we would have if the sound localisation was perfect.

Results

Sound source

A disadvantage of the smaller speaker is the maximum volume of it. This gives us a lower SNR than we would have had when we would use the bigger speaker. On the other hand, its maximum volume is still higher than the maximum volume of one single mosquito, so it has be possible to detect a signal from the smaller speaker, otherwise the bug zapper would not work 'in real life'.

When measuring far away (25-30 cm) from the microphones, there is no difference in the accuracy measurements between the two speakers. However, when it is moved closer to the microphones, the bigger speaker has a fluctuating, incorrect signal, while the smaller sound source still gives a reproducible measurement. Therefore we have chosen to use the smaller sound source with a diameter of 1.5 cm.

Microphones & calibration

As mentioned in the theoretical aspects, our first guess is to place the microphones around the space that is measured in, because it could be possible that the result gets better by the spread in the microphones along the different axes. In figure 7 below, the measured DDOAs and the expected DDOAs are shown for six different positions. The measurements in this graph are shown without error bars, but these are very small. The measurements in the DDOA do not fluctuate more than ± 0.05 cm.



Figure 7: Measured DDOAs compared to the expected DDOAs for the first set-up at six different locations.

The shape of the graphs is almost the same for the expected and the measured values, but there is a systematic error, which is much bigger than the one that Ruud van Laar and Martijn van der Ouderaa found in their set-up. [1]. While measuring the DDOAs, we had a small measurable space, so we decided to design a new set-up almost similar to the original set-up from Ruud van Laar and Martijn van der Ouderaa. [1]

So in our next set-up, we placed the microphones behind the space we measured in. This gives the DDOAs as shown in figure 8 below. Here we see that the systematic error in the measurements is smaller, but we also see that there are more unexpected measurements, especially for microphone 3 and 4, these measurements do not seem to have a constant mistake in the DDOA. Since microphone 3 and 4 are further away from the reference microphone, we will try a third set-up, which is more similar to the set-up of the previous experiment. We place all of the microphones behind the measured space, but we bring them closer together, with a distance to the reference microphone of 15-20 cm.



Figure 8: The measured and expected DDOAs for the second set-up at twenty different positions

The third set-up gives us the results that are shown in figure 9. It can be seen that the systematic error decreases as the distance to the reference microphone decreases, but it is hard to say which set-up is the best.



Figure 9: The measured and expected DDOAs for the third set-up at twelve different positions

Beside the measurements of the DDOA, there is another difference between these three different set-ups. The first set-up cannot measure the same points as the second and third set-up, because the two microphones that are placed in the space we would like to measure are not infinitely small. The microphones are little boxes and therefore distort the wave front so the sound source cannot be considered as a point source when the sound source is behind the microphone.

We calculate the average of the difference between the expected and the measured DDOA to estimate the systematic error and the standard deviation to choose between the second and third set-up, the results of this calculation are shown in the table in figure 10. The second set-up has a smaller measurable space, but might be more accurate compared to the third set-up.

	Second set-up		Third set-up	
	Average (cm)	Stand. Deviation (cm)	Average (cm)	Stand. Deviation (cm)
DDOA1	-0.6	3.5	-0.6	3.9
DDOA2	-0.6	4.6	-2.5	3.4
DDOA3	-2.7	6.2	-1.0	4.1
DDOA4	-3.6	9.1	1.2	2.8

Figure 10: Table with average systematic errors and standard deviations.

The standard deviation is in both cases too big to get an accurate and precise result, so we will neglect a few of our measurements. This might sound a bit unusual, but it is possible that these locations were just out of our measurable space. The measurements we removed are all on the edge

of the space we measured in. In figure 11 and 12 the graph with only the measurable locationsⁱⁱ and the table with the averages and standard deviation are shown. We will not use the second set-up, since the standard deviation in the second set-up is bigger than the standard deviation in the third set-up.



Figure 11: Measured and expected DDOA for the third set-up - only the measurable locations.

	Average (cm)	Standard Deviation (cm)
DDOA1	1.5	0.6
DDOA2	-1.6	1.0
DDOA3	0.2	1.1
DDOA4	1.1	1.0

Figure 12: Systematic errors that will be used to correct the localisation measurements in the third set-up

These results are good enough to use, but we still have more fluctuations than we had in the first setup, where the microphones surrounded the space. Therefore we have designed a fourth set-up with the microphones surrounding the space we would like to measure in, a little bit different from the first set-up. We choose to make the space between the microphones bigger, in order to have the same measurable space as with the second and third set-up. This gave the results from figure 13 and 14.

ⁱⁱ It is possible that at one location only one microphone is not measurable. The measurement of the DDOA is only dependent of the positioning of the reference microphone and the 'measured' microphone. Therefore we will end up with different numbers of measurements for the different microphones.



Figure 13: Measured and	expected DDOA for the	e fourth set-up - onl	y the measurable locations.

	Average (cm)	Standard Deviation (cm)
DDOA1	0.04	0.51
DDOA2	-1.17	0.56
DDOA3	-0.65	0.73
DDOA4	-0.07	0.93

Figure 14: Systematic errors that will be used to correct the localisation measurements in the fourth set-up

After analyzing the second, third and fourth set-up, it is still hard to choose between those two. Working through the error analysis of the algorithm we used [3], shows us that the relative mistake in the DDOA is important for the accuracy of the calculation of the location. Therefore, we will use the third and fourth set-up and choose the best, since the mistake in the DDOA is relatively small compared to the DDOA for both set-ups.

Sound localisation

To determine how well the described set-ups work, we located the sound source at 18 different positions and measured the x-, y- and z-position of the source and compared this to the results of the sound localisation. The results for the third set-up are shown in figure 15 on the left. The results for the fourth set-up are shown in the graph below on the right.





It can be seen that the measurements with the surrounding microphones are more precise than the measurements with the microphones at y-z plane, especially in the x-direction. We can also see that the fourth set-up has a smaller measurable range, because the mistake in the localisation at the edge of the space is much bigger than the error at other measured points, as we already expected. If we neglect the points at the edge of our measured space we get the results from figure 16.

The fourth set-up has some advantages compared to the second and third set-up. The microphones are further away from each other, so the relative error is smaller and since they are more spread in the three directions, the errors are smaller for each of the directions.



Figure 16: Comparison of the real and measured position of the sound source, with only the measurable points from the fourth set-up. Real position marked using a red star, the blue line indicates where the point was measured.

In the figure above the localisation of the measurable locations is shown. The average error in the xdirection is 1.1 cm (maximum 3.5 cm), in the y-direction it is 0.6 cm (maximum 2.6 cm) and in the zdirection it is 1.0 cm (maximum 2.4 cm). The measurable space is approximately spherical, with a diameter of 15-20 cm.

At first sight this might sound unsatisfying, because we did not improve the localisation as much as we hoped. On the other hand, our measurements are not averaged over multiple measurements, so we did reduce the processing time.

It seems like we will not hit every mosquito that comes into our bug zapper, but actually every mosquito will be measured more than once when it flies through our measurable space. We will further analyse the chance of surviving after the analysis of the galvano-mirrors when we combined the two systems.

Galvano-mirrors

Various characteristics of the signal have been measured for twelve different frequencies (25Hz up to 300Hz in steps of 25Hz) and five different step amplitudes. The step amplitude is given in the angle between the start and end position of the galvano-mirror. As said before, the delay of the galvano-mirror is the phase difference between the triangular function and the square wave, the settling time is the time it takes to coincide with the input value. A typical response can be seen in figure 17. These characteristics are measured at the top and the bottom of the step function, in figure 17 a measurement at the top of the step function is shown.



From these responses the average settling time and the average delay of the galvano-system are calculated, the settling time as a function of the amplitude is shown in figure 18, the delay in the galvano-mirror as a function of the amplitude is shown in figure 19 and the total response time as a function of the amplitude is shown in figure 20.



Figure 18: Settling time as function of the step amplitude



Figure 19: Galvano-delay as function of the step amplitude



Figure 20: Total response time as function of the step amplitude

The first thing that we see from the three figures above is that the response time depends on the direction of the step. This simply shows that the feedback of the galvano is not symmetric, this can also be seen directly on the screen: at the bottom there is a slight overshoot increasing in size at higher frequencies. The second thing that we conclude from these graphs is that the two physical systems are not the same, because there is a difference in the response time between the two axes.

The delay of the triangular signal has been measured as well. In order to have an accurate timing the optical path was increased to about 3 m giving an image width or height of about 1 meter. This has been done because the beam is at shorter optical path lengths longer on the photodiode, making it harder to accurately measure the delay because the time on the photodiode can be of the same order as the delay. The delay has been measured at 100Hz and is shown in figure 21. There is a small error in this delay because of the time the laser is on the photodiode, this was about 25 μ s.

The settling time of the DAQ has been measured to be about 15 μ s, making it for practical purposes small enough to be neglected.

Axis	Delay
X-axis	290±7 μs
Z-axis	280±5 μs

Figure 21: Delay of the triangular signal

All these measurements combined show that there is an input delay in the square wave of about 0.1 ms. The settling time, excluding this input delay is about 0.6 ms.

The static behaviour of the galvano-mirrors has been measured as well. The results of these measurements are shown in figure 22. The maximal deviation from the linear fit is about 0.7 mm, which is about half of the beam size, so we can assume that the galvano-system has a linear response over this voltage range.



Figure 22: Deflection as function from the input voltage at 42,8 cm away from the galvano-mirrors.

Complete device

We have analysed 60 shots of the twenty random paths. We can conclude that 8% of the measurements will actually hit a mosquito, 44% is really close and might hit it if the mosquito flies in the right direction and 48% does not hit the mosquito.

In the 26 random 'walks' through our measurable space, the sound source is shot during 22 paths, which gives us a success rate of 85%. A random 'walk' is a path through the measurable space of approximately 20 cm.

Discussion

Sound source & sample

The sound sample we used during our measurements was a short sample from a mosquito with malaria. Different species of mosquitoes flap their wings at other frequencies, but they might also have other frequencies when they make a turn or change their speed. To check whether this is the case, one could try to use the designed system with real mosquitoes. This also would solve the next question: is the sound of the mosquito loud enough to be detected by the five microphones? The Signal to Noise Ratio we had was relatively high, because we worked in a quiet place and did not talk during our measurements, so the system might be not functional in a crowded place.

Sound localisation

The sound source localisation method we used, was chosen because of the good results Ruud van Laar and Martijn van der Ouderaa had with these results. They tried one other algorithm, which was too slow. Though the algorithm is known as a fast method to calculate the location, there might be a faster algorithm.

Another disadvantage of this algorithm is the fact that it can only detect one mosquito at a time. Even worse, it cannot measure the location of one of the mosquitoes in the measurable space if there are more than one, because the correlation will be inflected by the different sound sources.

Galvano-mirrors

There were a few disadvantages of the galvano-system we used. The first problem was that the space you could aim the laser in depends on the angle of the mirrors, but the maximum amplitude we had was not big enough. However, if we would have had bigger amplitudes, the mirror would not be big enough to reflect the beam at high angles. To increase this space, we tried to put the galvano-system further away from the measurable space, but this would not be very useful in real life, since one would like to have the device as small as possible.

However, the response time and the precision of the galvano-system was very good, so maybe one could try to design a system with multiple galvano-systems to increase the space that can be hit or use optical demagnification.

Processing time

The total processing time is 0.0198 sec, which includes the recording of the sample of the mosquito, which is 0.01875 sec. This is 98% of the total processing time, therefore we cannot reduce the processing time significantly without lowering the precision, because the length of the sample determines the precision of the correlation. The original processing time of the set-up from Ruud van Laar and Martijn van der Ouderaa was 2.5 seconds, but they only calculated the location. Our time to calculate the location is 0.0191 seconds, so we are 130 times faster.

Laser

Since we only did a proof of concept in the first place, we did not look at the laser we would need to actually kill a mosquito. The amount of energy you need to kill a mosquito is 100 mJ according to E. Johanson[5], from which we can conclude that we would need a 100W laser, which is not eye safe. However, we have only found one article about the energy you would need to kill mosquitoes, which might not be trustworthy and they do not give enough details about the exposure time. To make a functional bug zapper more research to this laser would be needed. It is important to know how much power as a function of the exposure time is needed to kill a mosquito.

Complete device

In our set-up, we can do 21 measurements while the mosquito travels 20 cm. The chance on a successful measurement is 8%, which means that the chance of survival for the mosquito is theoretically about 17% after the 21 attempts to kill it. The measured chance of survival is 15%, which is lower than you should expect at first sight. However, we still have those measurements that might hit the mosquito if it is travelling in the right direction, which makes it reasonable to believe that the chance of survival is only 15%.

Conclusion

We determined that with the described set-up it is possible to point a laser on the location of a sound source as long as its speed is not too high, though the accuracy is not very high.

Inaccurate measurements are mostly due to the sound localisation and not to the positioning of the laser. The measurements for the sound localisation can be done with 1 cm accuracy, which is too high to hit the mosquito every measurement. Eight percent of the measurements are precise enough to hit the mosquito.

The total success rate of our device is 85%, since we are able to do multiple measurements of each mosquito that goes through the measurable space.

Recommendations

During our project, we improved the bug zapper and proved that it is possible to pinpoint a source with a laser beam after determining the location. However, there are still some aspects of the bug zapper that could be improved.

- The measurable space is only a sphere with a diameter of 15-20 cm, more mosquitoes will be killed if this space is bigger.
- If there are two mosquitoes in (or close to) the measured the space, the system is unable to locate and shoot them, because the two signals will interfere. There might be a good solution to distinguish the two signals and locate them separately, but our set-up does not have this yet. To distinguish the two signals you might need more microphones and another algorithm than we used in our set-up, but the biggest problem will be the processing time of this new algorithm.
- In order to hit faster moving bugs, the processing time should be reduced even more, but this will have consequences for the accuracy of the measurements, as mentioned in the discussion.

There are also a few aspects that have to be considered before one should use this device in real life situations:

- If a mosquito is located, the laser will point at its location and will try to shoot the mosquito. If there is something on the path of the laser beam between the galvanomirrors and the mosquito, this will be hit first. The laser you'll need to kill mosquitoes will cause burns to other animals and humans as well. The system is therefore currently not suitable to use in your home. Maybe it is possible to use a sort of box around the system to protect the environment against the laser.
- The measurable space is still very small, but the space that the laser can hit is even smaller. To increase this space you should put the laser further away, but this will increase the size of the complete device. Most of the times your customers will desire a smaller device, since they try to save space in their house. Another good reason to try to keep the device small is the laser you are using to kill the mosquitoes. As said before, it is not eye safe, so we would like to limit the space this laser is used in.

List of abbreviations

TDOA	Time Difference Of Arrival
DDOA	Distance Difference Of Arrival
DAQ	Data Acquisition

References

[1] M. van der Ouderaa and R. van Laar, "The Bug Zapper", Bachelor's report University of Twente, 2013

[2] Alex Reisner, "Speed of Animals", http://www.speedofanimals.com/animals/mosquito

[3] M. D. Gillette and H. F. Silverman, "A Linear Closed-Form Algorithm for Source Localisation From Time Difference of Arrival", *IEEE signal processing letters*, vol. 15, pp. 1-4, 2008.

[4] R. H. Campbell, Composer, "Analysis of Mosquito Wing Beat Sound". [Sound Recording]. Worcester Polytechnic Institute. 1996.

[5] E. Johanson, "Mosquito Blaster," Make magazine, volume 23, pp. 48-53, 7 2010